

The 11th Society of Petroleum Engineers Comparative Solution Project: Problem Definition

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Summary

This article contains the description of, and call for participation in, the 11th Society of Petroleum Engineers Comparative Solution Project (the 11th SPE CSP, <https://spe.org/csp>). It is motivated by the simulation challenges associated with CO₂ storage operations in geological settings of realistic complexity. The 11th SPE CSP contains three versions: Version 11A is a 2D geometry at the laboratory scale, inspired by a recent CO₂ storage forecasting and validation study. For Version 11B, the 2D geometry and operational conditions from 11A are rescaled to field conditions characteristic of the Norwegian Continental Shelf. Finally, for Version 11C, the geometry of Version 11B is extruded to a full 3D field model. The CSP has a two-year timeline, being launched at the 2023 SPE Reservoir Simulation Conference and culminating at the 2025 SPE Reservoir Simulation Conference. A community effort is run in parallel to develop utility scripts and input files for common simulators to lower the threshold of participation; see the link to supplementary material on the CSP website. At the time of writing, complete input decks for one simulator are already ready for all three versions.

Introduction

Safe and efficient implementation of geological carbon storage (GCS) necessarily relies on reservoir simulators applied to uncertain geological data. While the strengths and limitations of reservoir simulation are well appreciated within petroleum production, GCS raises new challenges both in terms of physical processes and timescales. As an example, the enhancement of dissolution from a CO₂-rich supercritical phase to the aqueous phase through convective mixing ensures important long-term storage security, relevant on timescales from decades to centuries.

One consequence of the relative youth of the GCS industry, combined with the long timescales and new physical processes of interest, is that available field data for validation of simulation technology is still rare. This increases the importance of validation against proxy systems and code verification through comprehensive benchmarking efforts among simulators.

Background and Motivation. During 2021–22, three of the present organizers led a forecasting and validation study within the academic GCS community (Nordbotten et al. 2022; Flemisch et al. 2023), as illustrated in **Fig. 1**. The primary intent was to validate the long-term performance of numerical simulators for GCS, with particular emphasis on the post-injection period, and to assess the ability to state accurately well-calibrated forecasting intervals. The study also revealed several numerical challenges, both in terms of numerical accuracy when resolving the reservoir dynamics and in terms of obtaining good solver performance [see, e.g., Flemisch et al. (2023); Saló-Salgado et al. (2023); Wapperom et al. (2023)].

Separately, the development of numerical simulation capabilities for subsurface applications has historically benefited substantially from common reference simulation cases, notably the series of 10 CSPs organized within the SPE between 1981 and 2001 [see Islam and Sepehrmoori (2013) for a review]. These observations provided the initial motivation for developing a set of benchmark cases for CO₂ storage within the concept of a new SPE CSP.

In developing this 11th SPE CSP (<https://spe.org/csp>), we hope to provide a common platform and reference case for numerical simulation of GCS. Specifically, we anticipate that the following topics will be discussed relative to this baseline:

- Development and verification of accurate and efficient discretization methods for multiphase, multicomponent flow and transport.
- Development and verification of space–time adaptive gridding and domain decomposition methods.
- Development of upscaling methods for convective mixing and dispersion in the context of CO₂ dissolution into water.
- Development and verification of robust and efficient linear and nonlinear solvers and solution and timestepping strategies for 2D and 3D at laboratory and field conditions and well models.
- Assessment of the importance of physical processes omitted from this study, including (but not limited to) geochemical reactions, mechanical response, and more realistic boundary conditions.

Furthermore, as of the date of launching this CSP, we do not anticipate that a fully converged solution (in the sense of grid refinement) will be achievable for any of the three versions of the CSP by means of standard numerical methods on desktop hardware. This anticipation is justified in part based on the experiences from the previous academic benchmark cited above and in part due to the known challenges associated with accurately simulating the dissolution and convective mixing of CO₂ into water, in particular outside the context of

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Original SPE manuscript received for review 15 June 2023. Revised manuscript received for review 12 October 2023. Paper (SPE 218015) peer approved 17 October 2023. This paper is published as part of the 11th Comparative Solution Project Special Issue.

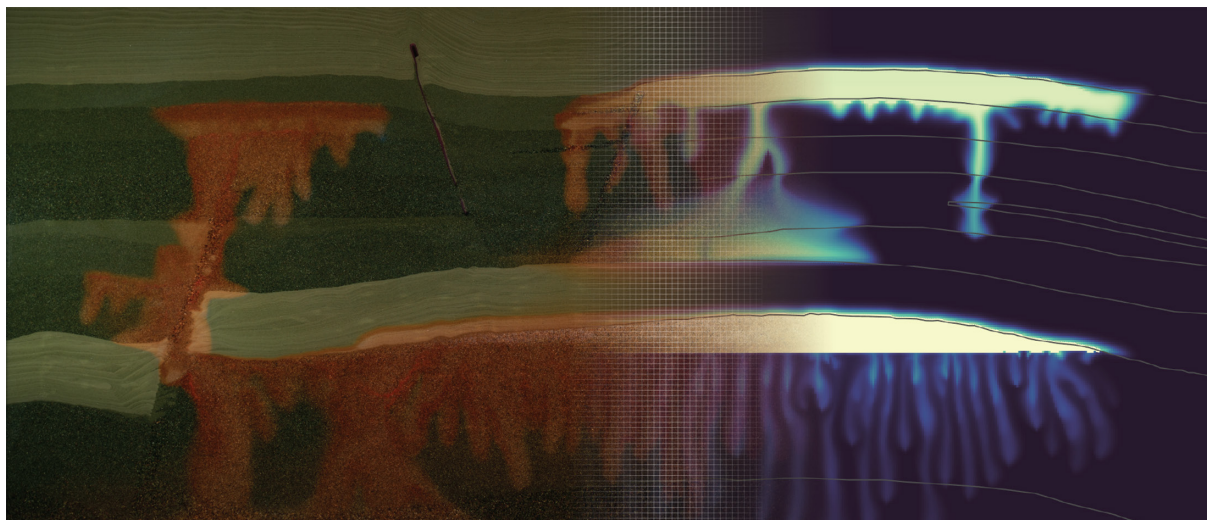


Fig. 1—Illustration containing a collage of a laboratory experiment (left, see Fernø et al. 2023) and a numerical simulation (right, see Saló-Salgado et al. 2023) on the same geometry as SPE CSP 11A.

trivial geometries; see, for example, Pau et al. (2010). As such, providing a reference solution to this CSP is a challenge in itself that will likely require advanced methods and high-performance computing.

CSP Overview. This 11th SPE CSP (<https://spe.org/csp>) is based around a synthetic geological cross section, representative of the structures found in the Norwegian Continental Shelf. The cross section is defined in terms of seven facies and is used to realize three versions of the CSP: Version 11A is defined as a 2D experiment at laboratory scale and surface conditions. Version 11B is defined as a 2D transect at field scale and conditions. Version 11C is a 3D extrusion of Version 11B, thus corresponding to a full synthetic field study. The three versions (11A, 11B, and 11C) all contain different challenges and should not be considered to be of increasing difficulty. *Indeed, many may find Version 11B to be the easiest, and we recommend starting with this case.*

A common 2D transect geometry is utilized for all three versions of the CSP and is designed to strike a balance between (a) simplicity of definition, (b) geological and operational realism, and (c) providing several key computational challenges associated with numerical simulation of CO₂ injection, migration, and long-term storage in water-filled porous media.

We recognize that to provide a successful CSP, a balance needs to be attained between including a maximum amount of geological, operational, and physical realism versus a CSP that can be well addressed by a broad spectrum of the community. Such considerations permeate the whole development of this CSP, and some of our main considerations are highlighted as follows.

- **Geologic realism:** Our goal has been to provide a geometry that is easy to understand and implement, that at the same time corresponds conceptually to a realistic geological formation in the Norwegian Continental Shelf. We have chosen to address this by using a common 2D transect in all three versions of the CSP, that itself was designed to balance complexity with computational addressability. This 2D transect is then stretched, extruded, and deformed between the three variants of the CSP.
- **Heterogeneity:** We have chosen to emphasize structural heterogeneity (facies and faults) over local-scale heterogeneity. This choice is justified by two considerations. First, local-scale heterogeneity is covered by the 10th SPE CSP. Second, we wish to have a CSP that in principle has a computable solution and can be reasonably well approximated by the majority of current simulators, but that would be prohibitive with fine-scale (or stochastic) heterogeneities.
- **Fluid complexity and geochemistry:** We have chosen to specify two-phase, two-component flow with thermal effects (Versions 11B and 11C only). This corresponds to pure water in the reservoir, with pure CO₂ injection. The omission of salts and other minerals in the system is in part due to the relatively poor characterization of the properties of brine-CO₂ mixtures in the literature, and to avoid modeling permeability as a function of salt precipitation and other geochemical processes. These choices substantially simplify the problem definition. The inclusion of thermal effects is an acknowledgment that CO₂ may frequently be injected at a temperature significantly below the reservoir temperature.
- **Geomechanics:** Geomechanics is not included in the CSP based on two arguments. First, the fluid-mechanical coupling is primarily a total pressure coupling, and we thus consider the multiphase flow processes to be a somewhat orthogonal challenge to poromechanics. As such, we believe they can be to a large extent studied separately. Second, we acknowledge that a substantial fraction of available reservoir simulators do not include a native coupling to mechanical response and wish that the CSP should also be open to these participants.
- **Petrophysical processes:** After careful consideration, we have chosen to include capillary forces and dispersion in the description but not relative permeability hysteresis. We justify this choice as we consider capillary forces and dispersion to have greater conceptual importance as they represent important terms in the governing equation during injection and post-injection, respectively, and as they are necessary for a grid-converged solution to exist. On the other hand, hysteresis is of lesser conceptual importance as it is a modification of existing constitutive laws.

The choices just described will invariably exclude the active research and development interests of many members of the community, and we therefore emphasize that this CSP is meant to be used as a common baseline, from which the incorporation of additional complexities, not included in the CSP, is more than welcome.

Both the injection protocol and the target quantities for the simulation are defined with operational realism in mind. In particular, simulation results are to be reported both in terms of spatial maps of the field variables (pressure, saturation, phase composition, and, for Versions 11B and 11C, also temperature). Furthermore, we request target quantities that represent proxies for assessing the long-term

security of carbon storage. These are motivated by the following key questions and variables, made precise in the sections “Measurables” and “Data Reporting”:

- P1. *As a proxy for assessing the risk of mechanical disturbance of the overburden:* Time evolution of pressure at two observation points.
- P2. *As a proxy for when leakage risk starts declining and our ability to simulate accurately phase partitioning:* Time evolution of phase partitioning of CO₂ within a region covering the primary storage dome.
- P3. *As a proxy for our ability to handle more complex geological features:* Time evolution of phase partitioning of CO₂ within a region covering a secondary storage dome.
- P4. *As a proxy for our ability to capture onset of convective mixing:* Time evolution of a measure of density-driven fingers in a region below the gas-water interface of the primary storage dome.
- P5. *As a proxy for our ability to capture migration into low-permeable seals:* Time evolution of the total mass of CO₂ in the seal facies.

Community Resources. The current article constitutes the official CSP description. The development of this description has been paired with an ongoing community effort to develop utilities that lower the threshold for participation. This community effort is hosted at <https://github.com/Simulation-Benchmarks/11thSPE-CSP>, and at the time of writing contains:

- Geometry files and scripts for producing structured meshes for all versions of the CSP.
- Scripts for generating thermodynamic tables based on the NIST database.

Sample input files for common simulators are in development and corresponding input decks for one simulator are already available for all three versions of the CSP. We emphasize that the input decks are intended to support the participants in setting up their computational workflows. Especially, the contained grids are expected to be optimized by the participants for generating their respective CSP results.

Call for Participation and Timeline. Participation in this 11th SPE CSP is open to all interested parties, subject to the condition that the agreement of participation must be completed, signed, and submitted by 1 December 2023.

The CSP is planned according to a 2-year cycle, with tentative milestones as follows:

- 29 March 2023: Official announcement of the 11th SPE CSP at the 2023 SPE Reservoir Simulation Conference, Galveston, Texas, USA.
- 1 October 2023: Final date for publication of corrections or amendments to the CSP description (this article).
- 16–18 October 2023: Special session at the SPE Annual Technical Conference and Exhibition, San Antonio, Texas, USA.
- 1 December 2023: Open call for participation period ends.
- 1 March 2024: Deadline for submission of early CSP simulation results.
- March 2024: First intercomparison workshop for all CSP participants (virtual).
- 1 September 2024: Deadline for submission of final CSP simulation results.
- September 2024: Final intercomparison workshop for all CSP participants (hybrid).
- December 2024: Completion of draft report on the results of the CSP.
- February 2025: Report on the results of the CSP finalized and submitted.
- March 2025: Special session at the 2025 SPE Reservoir Simulation Conference.

Early Access Team. The authors thank and acknowledge the contributions of the “Early Access Team”:

- Norwegian Research Center (NORCE): Tor Harald Sandve and David Landa Marban
- SINTEF Digital: Halvor Møll Nilsen, Odd Andersen, Olav Møyner, and Vetle Nevland
- SLB: Marie Ann Giddins and Jarle Haukås
- Stuttgart University: Holger Class, Dennis Gläser, and Kai Wendel

The early access team has supported the development of the CSP through giving feedback on the CSP description, quality control of the proposed versions of the CSP, and providing supporting material in the form of example computational grids and run files. This team also formed the initial core of the community developing the resources mentioned in the section “Community Resources.”

Technical Description of CSP 11A

The CSP 11A is a 2D geometry set at laboratory scale and conditions. Version 11A is closely inspired by an actual CO₂ storage laboratory experiment; as such, there is a real-world model that provides insight into the general system behavior (Fernø et al. 2023). The distribution of gas-phase CO₂ and dissolved CO₂ at the end of injection can be seen in Fig. 2.

Attempting to reproduce actual CO₂ storage experiments *in silico* is important to assess the predictive capabilities of simulators. The experiment underlying CSP 11A was conducted at atmospheric conditions, and this introduces challenges that will not necessarily be seen in simulations conducted at reservoir conditions, including large density differences between CO₂ and brine and diffusion being a determining factor for the onset and wavelength of the viscous fingers, as discussed in more detail by Wapperom et al. (2023). Version 11A will likely prove to be more difficult to simulate than Version 11B, and even though we describe most of the general setup of the CSP for Version 11A, we recommend Version 11B as a starting point for most participants.

Governing Equations and Constitutive Laws. As governing equations, we state the standard isothermal two-phase, two-component extension of Darcy’s law. For a detailed description, refer to Nordbotten and Celia (2011) or Lake et al. (2014); the main equations are summarized below. We emphasize that all parameters and constitutive functions are defined as constants within each facies (see the geometry description in the next section and parameters in the section “Facies Properties”).

Multiphase Darcy’s law for phases $\alpha = n$ (CO₂-rich nonwetting gas phase) and $\alpha = w$ (H₂O-rich wetting liquid phase):

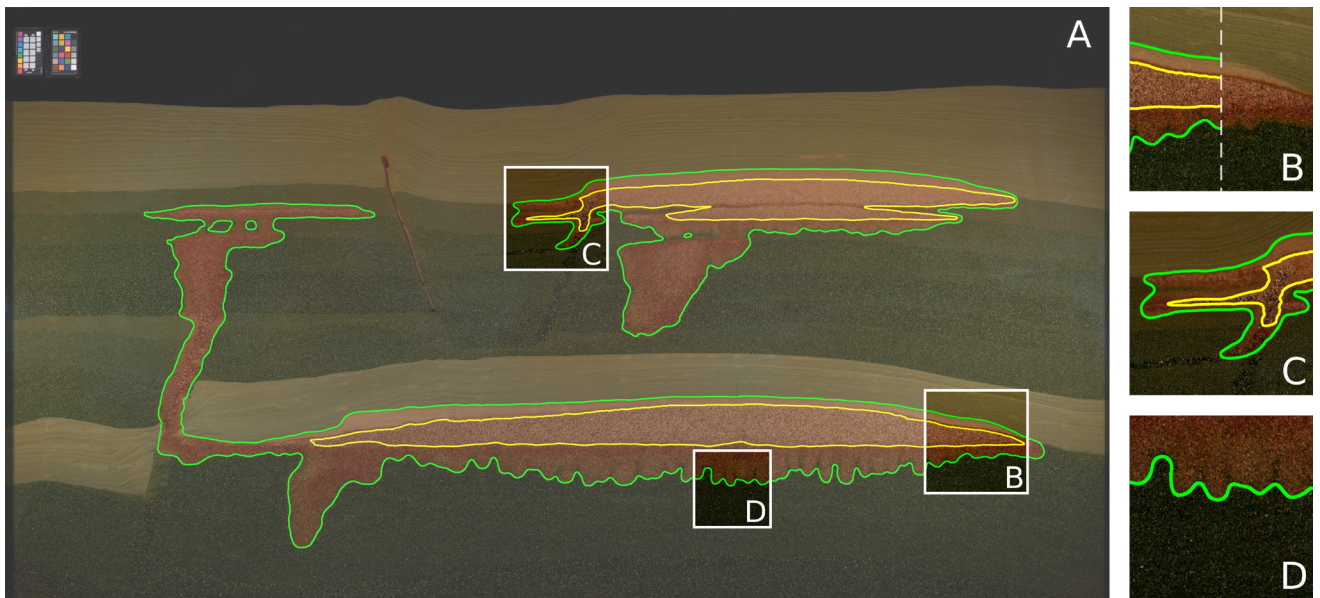


Fig. 2—Image of a physical laboratory-scale CO₂ storage experiment after about 5 hours, with contours of regions with mobile gas (yellow) and dissolved CO₂ (green) overlain, from Fernø et al. (2023).

$$\mathbf{u}_\alpha = -\frac{k_{r,\alpha}\mathbf{k}}{\mu_\alpha} (\nabla p_\alpha - \rho_\alpha \mathbf{g}). \quad (1)$$

Here, \mathbf{u}_α is the volumetric flux of phase α ; p_α is the phase pressure; $k_{r,\alpha}$ and \mathbf{k} are the relative and intrinsic permeabilities, respectively; μ_α is the phase viscosity; ρ_α is the phase density; and \mathbf{g} is the gravitational force, defined with three significant digits, $|\mathbf{g}| = 9.81 \text{ ms}^{-2}$, pointing “down.”

Component mass conservation for components $i = \text{CO}_2$ and $i = \text{H}_2\text{O}$:

$$\sum_{\alpha=w,n} \left[\frac{\partial (\rho_\alpha \phi s_\alpha \chi_\alpha^i J)}{\partial t} + \nabla \cdot (\rho_\alpha \mathbf{u}_\alpha \chi_\alpha^i + \rho_\alpha \mathbf{j}_\alpha^i) \right] = 0. \quad (2)$$

Here, ϕ is the porosity, χ_α^i is the component mass fraction in phase α , t is the time variable, and \mathbf{j}_α^i is the sum of diffusive and dispersive fluxes. Finally, J is a volumetric density term (i.e., reservoir volume per domain volume) that is used for adding volume to boundaries for CSP 11B and 11C. For this section, CSP 11A, $J = 1$, and can be omitted from the equations.

Diffusive and dispersive flux for component i in phase α :

$$\mathbf{j}_\alpha^i = - (s_\alpha \phi D_\alpha + E |\mathbf{u}_\alpha|) \nabla \chi_\alpha^i. \quad (3)$$

Here, D_α is the mutual diffusivity in phase α , while $E |\mathbf{u}_\alpha|$ is a linear dispersion model, with isotropic dispersivity E . The diffusive and dispersive fluxes are discussed in more detail in the section “Dispersion.”

Completeness of Model. For phases $\alpha = n, w$ and components $i = \text{CO}_2, \text{H}_2\text{O}$:

$$\sum_{\alpha=w,n} s_\alpha = 1 \text{ and } \sum_{i=\text{CO}_2, \text{H}_2\text{O}} \chi_\alpha^i = 1. \quad (4)$$

In addition to the governing equations provided above, the following constitutive laws are considered.

Relative Permeability. For primary drainage (initial period of injected gas displacing water), we consider normalized saturations:

$$s_{w,n} = \max \left(\frac{s_w - s_{w,\text{imm}}}{1 - s_{w,\text{imm}}}, 0 \right) \text{ and } s_{n,n} = \max \left(\frac{s_n - s_{n,\text{imm}}}{1 - s_{n,\text{imm}}}, 0 \right), \quad (5)$$

where $s_{\alpha,\text{imm}}$ is the saturation below which the phase is immobile. The Brooks-Corey relative permeability is given as a unique function of saturation by:

$$k_{r,\alpha}(s_\alpha) = (s_{\alpha,n})^{c_{\alpha,1}}. \quad (6)$$

Here, the exponents $c_{\alpha,1}$ determine the nonlinearity of the relative permeability.

Capillary Pressure. The phase pressures are related depending on saturation:

$$p_n - p_w = p_{\text{cap}}(s_w). \quad (7)$$

The basic Brooks-Corey capillary pressure is given by

$$\tilde{p}_{\text{cap}}(s_w) = p_{\text{entry}} \cdot (s_{w,n})^{-\frac{1}{c_2}}. \quad (8)$$

Here, p_{entry} is the entry pressure for the rock. We remark that capillary pressure is only physically meaningful when the phases are connected. For immobile wetting saturations, water connectivity is not sufficient for macroscopic fluid flow, and a unique wetting pressure is not defined from the basic Brooks-Corey curve. This has no impact on the flow calculations (because the wetting phase relative permeability is zero), but this will impact thermodynamical calculations. For this CSP, we resolve this issue by defining an extended capillary pressure, valid for all saturations, as

$$p_{\text{cap}}(s_w) = p_{\text{cap,max}} \cdot \text{erf} \left(\frac{\tilde{p}_{\text{cap}}(s_w) \sqrt{\pi}}{p_{\text{cap,max}}} \right). \quad (9)$$

Here, $p_{\text{cap,max}}$ defines a maximum capillary pressure, while the error function ensures a smooth transition of the capillary pressure function to the maximum value. For completeness, we emphasize that as the error function is defined as the integral of the normal distribution, it is well-defined at infinity: $\text{erf}(\infty) = 1$. Capillary pressure-saturation relationships are illustrated in the section “Facies Properties” and discussed in more detail in sections “Considerations for Version 11A” and “Vertical Equilibrium Pressure and Saturation Distribution.”

Thermodynamics. The description of the thermodynamics is split into three parts—phase partitioning, pure-phase properties, and mixture properties.

1. We define the phase partitioning of the pure CO₂-H₂O system according to Spycher et al. (2003); see in particular their Section 4.3 and Tables 1 and 2 therein. To be precise, we emphasize that for the purpose of this CSP, the solubility limits of each phase (i.e., CO₂ solubility limit in the water-rich wetting phase and the H₂O solubility limit in the CO₂-rich nonwetting phase) should be calculated based on the pressure of the same phase. Mass transfer between phases is assumed to be instantaneous at each point, immediately dissolving/vaporizing available CO₂ and H₂O until the solubility limit is reached.
2. The pure-phase CO₂ and H₂O properties are defined according to the NIST database, see <https://webbook.nist.gov/chemistry/fluid/> (Lemmon et al. 2089). The respective phase pressure is used when evaluating the pure-phase properties.
3. For the range of conditions considered herein, the mutual solubilities are quite small. Consequently, all mixture properties are considered equal to that of the pure phase except for water density, which takes the form (Garcia 2001):

$$\frac{1}{\rho_w(p_w, T, \chi_w^{\text{CO}_2})} = \frac{1 - \chi_w^{\text{CO}_2}}{\rho_w(p_w, T)} + \frac{\chi_w^{\text{CO}_2}}{\rho_{n,\phi}(T)}. \quad (10)$$

In this expression, $\rho_w(p_w, T, \chi_w^{\text{CO}_2})$ is the density of water containing $\chi_w^{\text{CO}_2}$, while $\rho_w(p_w, T)$ denotes the pure-phase properties discussed in Point 2 above. Finally, $\rho_{n,\phi}(T)$ is the apparent density of CO₂ dissolved in water [defined as $\rho_{n,\phi}(T) = M_2/V_\phi$ in the notation of Garcia (2001)]. This quantity is specified in Eq. 3 of Garcia (2001) and parameterized therein as

$$V_\phi = 10^{-6} \cdot (37.51 - 9.585 \times 10^{-2}T + 8.74 \times 10^{-4}T^2 - 5.044 \times 10^{-7}T^3), \quad (11)$$

where temperatures are measured in Celsius, and the molar weight of CO₂ is $M_2 = 44.01 \times 10^{-3}$ kg/mol. The gas density as well as both phase viscosities are unaffected by their composition.

Rock Compressibility. The rock is considered incompressible, thus ϕ does not vary over time.

Geometry, Boundary, and Initial Conditions. The geometric description is motivated by laboratory experiments relevant to North Sea storage formations and has been developed in consultation with faculty and researchers at the Department of Earth Science, University of Bergen.ⁱ The geometry presented here is a simplification of the geometry defined in Nordbotten et al. (2022).

The length of the porous medium is 2.8 m and the height is 1.2 m. Version 11A of the CSP is 2D, but to present quantities in common units of “mass per volume,” we consider a uniform depth in the third dimension of 0.01 m. The porous domain consists of the full porous medium, except for the two injection wells, as specified below.

Fig. 3 provides a sketch of the geometry; a precise definition is given in the gmesh-compatible file `spe11a.geo`, available as part of the benchmark description.ⁱⁱ As evident from the figure, the geometry contains seven facies, all of which are considered to be internally homogeneous. The facies properties are given in the next section.

The figure contains three boxes that are used for reporting. Their (x, z) coordinates are measured relative to the lower-left corner of the domain and are specified in terms of their bottom-left and top-right corners:

Box A: bottom left (1.1, 0.0), top right (2.8, 0.6)

Box B: bottom left (0.0, 0.6), top right (1.1, 1.2)

Box C: bottom left (1.1, 0.1), top right (2.6, 0.4)

The figure also indicates the presence of the two injection wells, with (x, z) coordinates:

Well 1: (0.9, 0.3)

Well 2: (1.7, 0.7)

Additionally, we consider two pressure observation points (POPs), with (x, z) coordinates:

POP 1: (1.5, 0.5)

POP 2: (1.7, 1.1)

For the simulation, we specify the following conditions:

Temperature. Isothermal conditions of 20°C are considered for CSP 11A.

Boundary Conditions. The left, right, and bottom boundaries are impermeable, that is:

ⁱA special thanks goes to Robert Gawthorpe, Atle Rotevatn, and Casey Nixon for their helpful comments.

ⁱⁱSee GitHub repository: <https://github.com/Simulation-Benchmarks/11thSPE-CSP/>

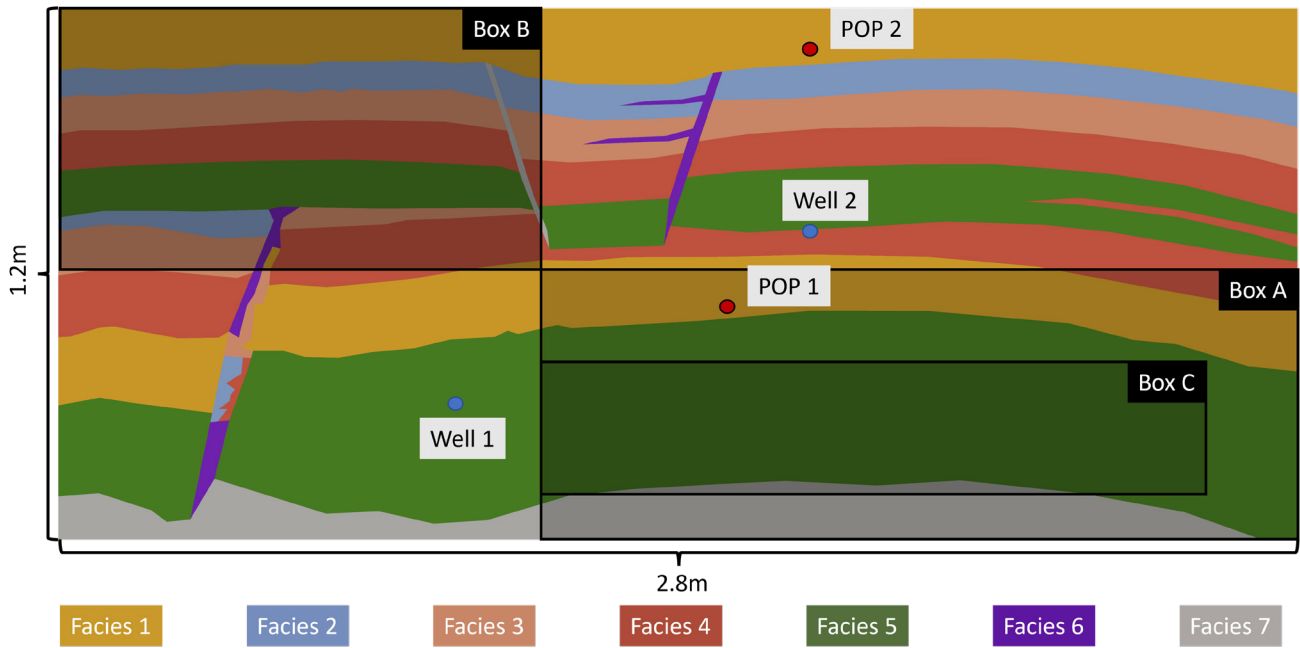


Fig. 3—A sketch of the benchmark geometry. The geometry includes an anticline (right side), where CO₂ accumulation is anticipated. There are three fault-like structures in the geometry, with different permeabilities (two high and one low). The lower fault (left side) is heterogeneous and consists of several facies. The upper-left fault is a homogeneous sealing fault. The upper-right fault is homogeneous, consisting of a single facies. There are two CO₂ injection wells (blue circles) and pressure observation points (POPs, red circles) with locations given in the text. Boxes A, B, and C indicated in the figure correspond to regions of interest motivated in the section “CSP Overview” and further detailed in the section “Measurables,” with positions defined in the text. The facies are identified by colors, and further detailed in the section “Facies Properties.”

$$\mathbf{u}_\alpha \cdot \mathbf{n} = 0 \text{ and } \mathbf{j}_\alpha^i \cdot \mathbf{n} = 0, \quad (12)$$

where \mathbf{n} is the (outward) normal vector to the boundary.

The top boundary is considered a constant pressure boundary in contact with pure water, that is:

$$p_w = p_{w,0}, \quad s_w = 1, \text{ and } \chi_w^{\text{H}_2\text{O}} = 1. \quad (13)$$

Here, $p_{w,0}$ is the boundary pressure, defined as $p_{w,0} = 1.1 \times 10^5$ Pa.

The two injection wells for pure CO₂ injection, $j = 1, 2$, are also defined as (internal) boundary conditions. Both wells are defined to have a radius of $r = 9 \times 10^{-4}$ m, centered at their respective coordinates. We refer to the respective well-to-reservoir circular boundaries as Γ_i , where we impose the boundary conditions:

$$X_n^{\text{CO}_2} \rho_n \mathbf{u}_n \cdot \mathbf{n} = \frac{Q_j(t)}{2\pi r}, \quad \mathbf{u}_w \cdot \mathbf{n} = 0, \quad \mathbf{j}_w^i \cdot \mathbf{n} = 0. \quad (14)$$

Here $Q_j(t)$ are the injection rates per unit depth (injection rate per well length for 11C), specified in the section “Operational Conditions.” The injection is pure CO₂, thus Eq. 14 is complemented by:

$$\begin{aligned} X_n^{\text{CO}_2} &= 1 \text{ if } Q_j(t) > 0 \\ \mathbf{j}_n^i \cdot \mathbf{n} &= 1 \text{ if } Q_j(t) = 0. \end{aligned} \quad (15)$$

Initial Conditions. The initial conditions represent a water-filled medium at rest, compatible with the boundary conditions, that is:

$$s_w = 1, \quad \chi_w^{\text{H}_2\text{O}} = 1, \text{ and } \mathbf{u}_\alpha = 0, \quad (16)$$

Facies Properties. The geometry contains seven facies: one seal (Facies 1), five permeable reservoir sands (Facies 2–6), and one impermeable (Facies 7). These provide the definition of the material properties, as given in **Tables 1 and 2**. These properties are consistent with laboratory-measured parameters for unconsolidated sands (Nordbotten et al. 2022; Fernø et al. 2023).

	Isotropic Intrinsic Permeability, k (m ²)	Porosity, ϕ (-)	Immobile Wetting Phase Saturation, $s_{w,imm}$ (-)	Gas-Entry Pressure, p_{entry} (Pa)	Diffusion Constants, D_w (m ² s ⁻¹)	Diffusion Constants, D_g (m ² s ⁻¹)
Facies 1	4×10^{-11}	0.44	0.32	1500	10^{-9}	1.6×10^{-5}
Facies 2	5×10^{-10}	0.43	0.14	300	10^{-9}	1.6×10^{-5}
Facies 3	1×10^{-9}	0.44	0.12	100	10^{-9}	1.6×10^{-5}
Facies 4	2.0×10^{-9}	0.45	0.12	25	10^{-9}	1.6×10^{-5}
Facies 5	4×10^{-9}	0.43	0.12	10	10^{-9}	1.6×10^{-5}
Facies 6	1×10^{-8}	0.46	0.10	1	10^{-9}	1.6×10^{-5}
Facies 7	0	0	N/A	N/A	0	0

Table 1—Properties for 11A that vary between facies.

Immobile gas saturation, $s_{n,imm}$ (-)	0.10
Max capillary pressure, $p_{cap,max}$ (Pa)	9.5×10^4
Shape exponent capillary pressure, c_2 (-)	2
Shape exponents relative permeability, $c_{\alpha,1}$ (-)	2
Dispersivity, E (m)	10^{-2}

Table 2—Properties for 11A that are equal in all facies.

We remark that the maximum capillary pressure is chosen to avoid any potential for a phase transition from water to vapor. As examples, capillary pressure and relative permeability functions are given in Fig. 4.

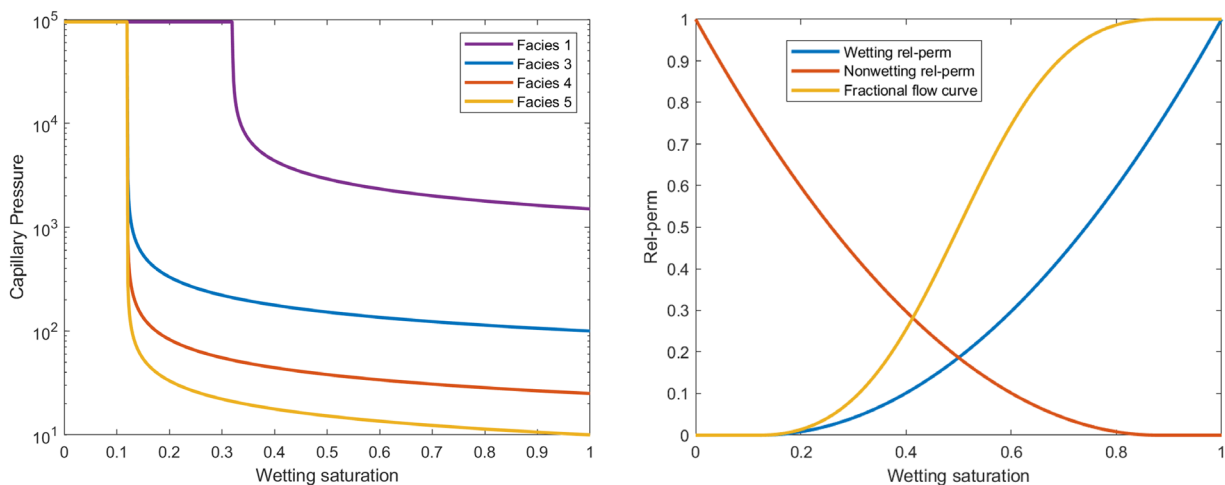


Fig. 4—Left: Capillary pressure for Facies 1, 3, 4, and 5, as function of wetting saturation. Right: Relative permeability and fractional flow for Facies 5, also as function of wetting saturation.

Operational Conditions. CO₂ injection protocol:

1. CO₂ injection in Well 1 with rate $Q_1(t) = 1.7 \times 10^{-5} \text{ kg s}^{-1} \text{ m}^{-1}$ for $0 < t < 18,000$ seconds (continuous injection for 5 hours).
2. CO₂ injection in Well 2 with rate $Q_2(t) = 1.7 \times 10^{-5} \text{ kg s}^{-1} \text{ m}^{-1}$ for $9,000 \text{ seconds} < t \leq 18,000$ seconds (start after 2.5 hours, end 2.5 hours later).
3. Monitor CO₂ flow and transport until final time $t = 432,000$ seconds (total run time of 5 days).

We emphasize that to obtain 3D rates, one must multiply by the nominal thickness of the geometry; thus the injection rates correspond to $1.7 \times 10^{-7} \text{ kgs}^{-1}$. Exemplifying these injection conditions, the specified mass rate corresponds to a volumetric rate of about 5 cm³ per min at 20°C and 1.1×10^5 Pa.

Measurables. In addition to spatial maps of the field variables, the following measurables shall be reported, details of which, including time resolution, are described in the section “Data Reporting.” These measurables correspond to proxies for the motivating questions in the section “CSP Overview.”

Pressure (Proxy P1). Pressure shall be reported at each of the two POPs (POP 1 and POP 2) in Pascals (Pa).

Phase Composition (Proxies P2 and P3). The distribution of the CO₂ phase shall be reported within boxes labeled A and B in Fig. 2. The phase distribution (in kilograms) shall be reported in the following categories: (1) Mobile, free phase (CO₂ at saturations for which

the nonwetting relative permeability exceeds zero); (2) immobile, free phase (CO₂ at saturations for which the nonwetting relative permeability equals zero); (3) dissolved (CO₂ in water phase); and (4) sealed (CO₂ in any form in Facies 1). The sum of the three first categories (mobile, immobile, and dissolved) shall equal the total mass of CO₂ in the respective box.

Convection (Proxy P4). For the box labeled Box C in Fig. 2, the extent of convective mixing shall be reported as the integral of the magnitude of the gradient in the relative concentration of dissolved CO₂. In other words, given the mass fraction of CO₂ in water (χ_c^w) and the solubility limit denoted as $\chi_{c,max}^w$, the following quantity M shall be reported:

$$M(t) \equiv \int_{\text{Box C}} \left| \nabla \left(\frac{\chi_c^w}{\chi_{c,max}^w} \right) \right| dV. \quad (17)$$

This quantity corresponds to the normalized total variation of the concentration field within Box C and (taking into account the nominal depth of the geometry) has units of meters squared.

CO₂ in Sealing Units (Proxy P5). Similar to the section “Phase Composition (Proxies P2 and P3),” the total mass of CO₂ in all sealing units (CO₂ in any form in Facies 1) shall be reported in kilograms.

Data Reporting. All results data will be uploaded by the participants to the dedicated website provided by SPE. An account at spe.org is required for the upload process, which is described in detail on the website. At the end of the CSP, corresponding to the release of the final report, all submitted data will be made public.

The reported data will be analyzed in two respects, both in terms of an intercomparison of general numerical simulation capability (global spatial maps) and also in terms of our ability to correctly assess key properties of the system (the measurables outlined in the section “Measurables”). Consequently, we establish both a “dense” and a “sparse” reporting protocol.

Groups are encouraged to submit up to four results, if they deem it interesting, of which at least one should be representative of a computation that is reasonable within common reservoir engineering practice.

Sparse Data. All measurables identified in the section “Measurables” shall be reported at 600-second (10-minute) intervals starting at the initial injection and lasting 432,000 seconds (5 days). The data is expected in csv format in the file `spe11a_time_series.csv` of the form:

```
#t [s], p1 [Pa], p2 [Pa], mobA [kg], immA [kg], dissA [kg], sealA [kg], < same for B >, M_C [m], sealTot [kg]
0.000e+00, 1.234e+56, 1.234e+56, < ... >
6.000e+02, 1.234e+56, 1.234e+56, < ... >
...
```

according to the measurables defined in the section “Measurables.”

Dense Data. A spatial map of all field variables (pressure, saturation, phase composition) shall be reported for each hour from the injection start. While the computational grids are generated by the participants individually and should be chosen by each group as they find most appropriate, for cross-group comparison, the spatial maps shall be reported relative to a uniform Cartesian grid of 280 by 120 cells (0.01 m by 0.01 m grid cells from the bottom of the domain). For each temporal snapshot indicated by H hours, $H = 0, 1, 2, \dots$, cell values should be provided in csv format in a file `spe11a_spatial_map_<H>.h.csv` of the form:

```
#x [m], z [m], pressure [Pa], gas saturation [-], mass fraction of CO2 in liquid [-],
mass fraction of H2O in vapor [-], phase mass density gas [kg/m3], phase mass
density water [kg/m3], total mass CO2 [kg]
5.000e-03, 5.000e-03, 1.234e+56, 1.234e+56, < ... >
1.500e-02, 5.000e-03, 1.234e+56, 1.234e+56, < ... >
...
2.795e+00, 5.000e-03, 1.234e+56, 1.234e+56, < ... >
5.000e-03, 1.500e-02, 1.234e+56, 1.234e+56, < ... >
1.500e-02, 1.500e-02, 1.234e+56, 1.234e+56, < ... >
...
2.785e+00, 1.195e+00, 1.234e+56, 1.234e+56, < ... >
2.795e+00, 1.195e+00, 1.234e+56, 1.234e+56, < ... >
```

The origin of the coordinate system should be located in the lower-left corner with the x -axis positively oriented toward the right and the z -axis positively oriented toward the top. (The reported x - and y -values refer to the lower-left corners of each cell in the uniform report grid.) Moreover, note that intensive variables (pressure, saturation, and mass fractions) should be reported as cell-center values while extensive variables (total mass) should be reported as integral/average values for the cell.

Performance Data. Reporting of performance data is strongly encouraged to the extent possible, but not mandatory. Note that several reporting quantities may not be relevant for certain participating groups, depending on their choice of numerical method and solution strategy. Performance data should be reported in three categories: as time series (similar to sparse data in the section “Sparse Data”), as spatial maps (similar to dense data in the section “Dense Data”), and as a questionnaire. These are detailed below. The participants should stick to the prescribed format, particularly the number of columns in the csv files, even if not all requested values can be reported. A missing value should be indicated by n/a.

The participants are encouraged to provide time series at 600-second (10-minute) intervals starting at the initial injection and lasting 432,000 seconds (5 days). The data are expected in csv format in the repository in the file `spe11a_performance_time_series.csv` of the form:

```
#t [s], tstep [s], fsteps [-], mass [kg], dof [-], nliter [-], nres [-], liniter [-], runtime [s], tlincol [s]
0.000e+00, 1.234e+56, 1.234e+56, 1.234e+56, 1.234e+56, < ... >
6.000e+02, 1.234e+56, 1.234e+56, 1.234e+56, 1.234e+56, < ... >
...
```

The reporting quantities provided as time series are defined as

- **tstep:** Average timestep size over the last 600 seconds.
- **fsteps:** Number of failed timesteps over the last 600 seconds.

- **mass**: Mass balance (i.e., total mass of CO₂ in the domain plus any mass that has crossed the boundaries).
- **dof**: Average number of degrees of freedom per timestep over the last 600 seconds.
- **nliter**: Total number of nonlinear iterations for all timesteps (both failed and converged) used to advance the solution in the last 600 seconds.
- **nres**: Number of local residual evaluations (e.g., per cell) for all timesteps over the last 600 seconds.
- **liniter**: Total number of linear iterations spent to advance the solution over the last 600 seconds.
- **runtime**: Total runtime for advancing the solution in the last 600 seconds. Details of the computational platform should be reported in the questionnaire, that is, type of hardware (CPU/GPU model and make, amount and type of memory, and memory bandwidth) and how it was used (number of threads/cores utilized, GPU offloading, etc.)
- **tlinsol**: Total time spent in the linear solver if applicable.

It is encouraged to include an extra file `spe11a_performance_time_series_detailed.csv` that reports the same quantities for all the timesteps and not just for the 600-second report steps.

The participants are encouraged to provide spatial maps for each hour from the start of injection. For cross-group comparison, the spatial maps shall be reported on a uniform Cartesian grid of 280 by 120 cells (0.01 m by 0.01 m grid cells from the bottom of the domain). For each temporal snapshot indicated by H hours ($H = 0, 1, 2, \dots$), cell values should be provided in csv format in a file `spe11a_performance_spatial_map_<H>.h.csv` of the form:

```
#x [m], y [m], cvol [m2], arat [-], C02 max_norm_res [-], H2O max_norm_res [-], C02
mb_error [-], H2O mb_error [-], post_est [-]
5.000e-03, 5.000e-03, 1.234e+56, 1.234e+56, 1.234e+56, <..>
1.500e-02, 5.000e-03, 1.234e+56, 1.234e+56, 1.234e+56, <..>
...
2.795e+00, 5.000e-03, 1.234e+56, 1.234e+56, 1.234e+56, <..>
<...>
```

The reporting quantities provided as spatial maps are defined as follows:

- **cvol**: Average geometric cell volume of the computational grid inside the given 1×1 cm cell of the reporting grid at the latest timestep.
- **arat**: Average aspect ratio (vertical/lateral) of the computational grid used inside the 1×1 cm reporting cell.
- **max_norm_res**: Maximum normalized residual within the 1×1 cm reporting box at the convergence of the latest timestep, defined for each component i as $\frac{\Delta t}{\sigma_i} \max_k \left| \frac{r_{i,k}}{\Phi_k} \right|$, namely, the maximum (over all computational cells k inside the reporting box) absolute value of the residual $r_{i,k}$ (the discrete version of the summand in Eq. 2) divided by the local pore volume Φ_k , multiplied by the timestep Δt , and divided by the surface density σ_i of the respective component (CO₂/H₂O). If this quantity cannot easily be computed for your numerical method, please specify how you define a similar measure in the questionnaire.
- **mb_error**: Mass-balance error within the 1×1 cm reporting box at convergence of the latest timestep, defined for each component i as $\frac{\Delta t}{\sigma_i} \frac{\sum_k r_{i,k}}{\sum_k \Phi_k}$, namely, the sum (over all computational cells k inside the reporting box) of the residuals multiplied by the timestep Δt and divided by the product of the pore volume of the reporting cell $\sum_k \Phi_k$ and the surface density σ_i of the respective component. If this quantity cannot easily be computed for your numerical method, please specify how you define the mass-balance error in the questionnaire.
- **post_est**: A posteriori estimate of the error between the computed and the true solution within the 1×1 cm reporting box at convergence of the latest timestep. Please specify how you define the error estimate in the questionnaire.

For both sparse and dense data, the participants are encouraged to add columns with extra performance metrics that are relevant for their solution approach. As an example, if adaptive implicit methods are used, extra performance data may be spatial maps of implicit/explicit variables. The reporting quantities above are supplemented by the questionnaire as given in **Table 3** (also available separately as `spe11a_questionnaire.xls`):

Question	Numerical Value (Where Applicable)	Free-Form Text Response (Where Applicable)
Simulator name, version, and reference		
Primary variables		
Spatial discretization		
Time discretization		
Linear solvers (incl. preconditioner)		
Notable aspects of solution strategy		
Specification of compute platform		
Resolution of ambiguities in the description		
Deviations from the description		
Any other comments		

Table 3—Questionnaire for supporting information to the CSP submissions.

Moreover, we strongly encourage all participants to provide as much additional data as possible that are helpful for the reproduction of the submitted results. This can be input decks for the performed simulations, source code, container images, etc. The information should be provided either in the form of persistent links to data (and software) published elsewhere or by uploading the data (and software) as supplementary material (maximum 100 MB) following instructions given on the CSP website (<https://spe.org/csp>).

Technical Description of CSP 11B

The CSP 11B is a 2D geometry set at field scale and conditions. No real analog exists, but the setup is typical of the Norwegian Continental Shelf and the scenario that the downscaled experiment underlying Version 11A sought to mimic. Many of the challenges from Version 11A carry over to Version 11B, although the balance of timescales between different processes is altered as one goes from laboratory conditions to field conditions; see discussion in Kovscek et al. (2023). A significant simplification of 11B relative to 11A lies in the higher density and lower compressibility of the CO₂-rich phase that make the system easier to solve numerically. We recommend that participants start with CSP 11B.

Version 11B nonetheless contains separate challenges. First, thermal effects are included. Furthermore, we emphasize again the challenge of capturing the onset and development of convective mixing accurately. Moreover, the injection of a relatively cool CO₂ supercritical phase will lead to potentially significant thermal effects in the near-well regions. Another challenge arises due to the boundary conditions, as Version 11B is essentially a closed system. The 2D nature of the domain, seen together with the lack of geomechanical response, therefore implies that some pressure buildup is to be expected.

Relationship to CSP 11A. The CSP 11B is a geometric scaling of CSP 11A, as illustrated in Fig. 5.

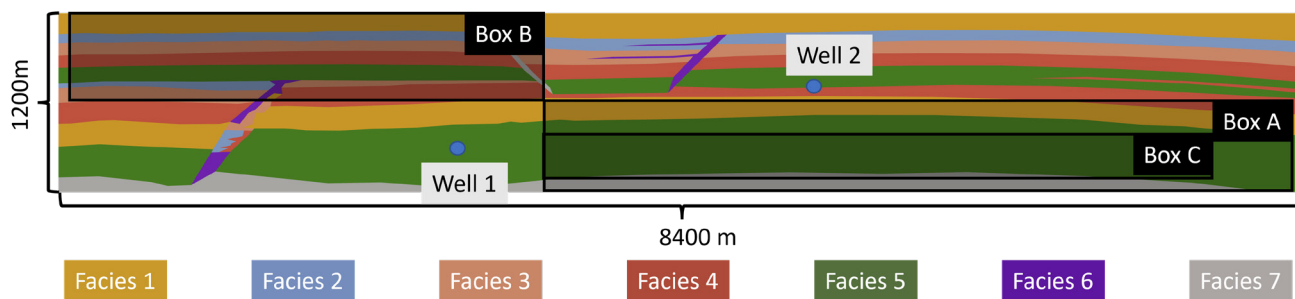


Fig. 5—Sketch of the benchmark geometry for CSP 11B, which is a scaling of the geometry in CSP 11A. For a detailed description, please refer to the caption of Fig. 3.

We summarize the commonalities and differences between CSPs 11A and 11B as follows:

1. The governing equations for CSP 11A apply to 11B, with the extension to thermal effects. Thus, the section “Governing Equations and Constitutive Laws” applies to CSP 11B, including the consideration of pure water (no salts).
2. A thermal equation is introduced for CSP 11B, as detailed below.
3. The geometry of CSP 11A is reused in CSP 11B, with the following scaling:
 - a. The horizontal scale (x -axis) is scaled at 1:3000.
 - b. The vertical scale (z -axis) is scaled at 1:1000.

Thus, the overall dimension of the CSP 11B is a vertical cross section measuring 8.4 km horizontally and 1.2 km vertically. We emphasize that we keep the coordinate system oriented with the vertical direction pointing “up” and the origin in the “lower-left” corner of the domain.
4. The geometric scaling applies also to the definition of Boxes A, B, and C and the well placements.
5. The only exception to the pure scaling of the geometry are the injection wells, which are kept circular, with a radius of 0.15 m.
6. As with CSP 11A, we assign a nominal depth to Version 11B of 1 m to allow us to work with volumetric quantities.
7. The initial and boundary conditions, together with the injection schedule, are updated to be consistent with field conditions; see specification below.
8. Facies properties are updated to be representative of field conditions; see specification below.

We define the three boxes in terms of their bottom-left and top right corners, stated as (x, z) (measured relative to the lower-left corner of the domain):

- Box A: bottom left (3300, 0), top right (8300, 600)
- Box B: bottom left (100, 600), top right (3300, 1200)
- Box C: bottom left (3300, 100), top right (7800, 400)

Note that in contrast to CSP 11A, Boxes A and B do not extend to the boundary. The reason for this will be clear in the section “Initial and Boundary Conditions.”

The two injection wells have (x, z) coordinates:

- Well 1: (2700, 300)
- Well 2: (5100, 700)

The two POPs have (x, z) coordinates:

- POP 1: (4500, 500)
- POP 2: (5100, 1100)

Furthermore, to avoid ambiguity, we define the following quantity:

One year is defined as exactly 365 days, containing 31,536,000 seconds.

Thermal Equations. Following the presentation in Lake et al. (2014), we give the thermal equation for multiphase flows in porous media as (with the omission of kinetic energy):

$$\sum_{\alpha=w,n,s} \frac{\partial}{\partial t} (\rho_{\alpha} \phi s_{\alpha} (e_{\alpha} - gz)) + \nabla \cdot (\mathbf{u}_{\alpha} (\rho_{\alpha} e_{\alpha} + p - \rho_{\alpha} gz) - \phi s_{\alpha} \kappa_{\alpha} \nabla T) = 0. \quad (18)$$

In this equation, we denote the solid phase by $\alpha = s$. As convention, set the “saturation” of the solid phase such that $\phi_{s_s} = 1 - \phi$ and its “Darcy flux” as zero $\mathbf{u}_\alpha = 0$. Furthermore, in Eq. 18, e_α is the internal energy per mass, while κ_α is the thermal conductivity. As in Eq. 2, J denotes reservoir volume per domain volume and will be detailed in the section “Initial and Boundary Conditions.”

Thermodynamics. The general thermodynamics defined in the section “Governing Equations and Constitutive Laws” also apply to CSP 11B, with the addendum that the internal energy and thermal conductivity of the wetting and nonwetting phases are considered independent of composition (i.e., $e_\alpha = e_\alpha(p, T)$, where the dependencies follow the same reference (NIST) as given in the section “Governing Equations and Constitutive Laws.”) For the solid phase, the internal energy is given in terms of temperature only, and is assumed to correspond to a constant specific heat capacity, that is:

$$e_s(T) = C_s T. \quad (19)$$

The specific heat capacity and the thermal conductivity are given in the section “Facies Properties.”

We remark that since we consider the internal energy of each phase as a function of pressure and temperature, Eq. 18 can be linearized to provide a temperature equation.

Initial and Boundary Conditions. We define initial and boundary conditions consistent with a depth of about 2000 m to the top of the defined geometry. Based on a presumed geothermal gradient of 25°C/km, we define the function $T_{\text{geo}}(\mathbf{x})$ for $\mathbf{x} = (x, z)$ as

$$T_{\text{geo}}(\mathbf{x}) = 70 - 0.025z. \quad (20)$$

Boundary Conditions. All boundaries are given no-flow boundary conditions for the fluid as stated in Eq. 12. For the energy equation, we consider an insulating boundary condition for the left and right boundary:

$$\mathbf{n} \cdot \nabla T = 0, \quad (21)$$

and constant temperature for the top and bottom boundaries; thus, for any point \mathbf{x}_B on the top or bottom boundary,

$$T(\mathbf{x}_B) = T_{\text{geo}}(\mathbf{x}_B). \quad (22)$$

To avoid an unphysical increase in reservoir pressure, we introduce additional volume at the horizontal boundaries. This is a variant of what is commonly known as pore volume multipliers, which are typically implemented by giving cells at the boundary of the domain an elevated volume content. Herein, we specify these conditions in rigorous mathematical terms as follows.

We define by $\ell_B(\mathbf{x}_B)$ (units of meters) the volume per area of the boundary. For any $\epsilon > 0$, we can extend this function to the whole domain, denoted L_B^ϵ , by using the notation $\mathbf{x}_B(\mathbf{x})$ to identify the closest point on the boundary to \mathbf{x} :

$$L_B^\epsilon(\mathbf{x}) = \begin{cases} \epsilon^{-1} \ell_B(\mathbf{x}_B(\mathbf{x})) & \text{if otherwise } |\mathbf{x}_B(\mathbf{x}) - \mathbf{x}| < \epsilon. \\ 0 & \end{cases} \quad (23)$$

In particular, the limit $L_B^0(\mathbf{x}) = \lim_{\epsilon \rightarrow 0} L_B^\epsilon(\mathbf{x})$ implies that L_B^0 is a Dirac-type distribution on the boundary with weight ℓ_B , where the extra volume is interpreted to lie “just inside” the boundary. We now formally augment the volume of the domain to include this extra volume, that is:

$$J(\mathbf{x}) = 1 + L_B^0(\mathbf{x}). \quad (24)$$

This has the effect of introducing an extra volume per area of ℓ_B immediately inside the boundary. The effect is that the boundary has the capacity to buffer fluids and energy, while all other aspects of the governing equations remain essentially unchanged. Importantly, the definition of the effective reservoir volume given in Eq. 22 can be approximated by using any finite value of ϵ , so that $J(\mathbf{x}) \approx 1 + L_B^\epsilon(\mathbf{x})$, and then implemented using a single layer of grid cells with this width.

The boundary volumes per area are specified as

- $\ell_B(\mathbf{x}_B) = 5 \times 10^4$ m for \mathbf{x}_B on the left and right boundaries, within Facies 2 through 5.
- $\ell_B(\mathbf{x}_B) = 0$ m for \mathbf{x}_B on the left and right boundaries, within Facies 1 and 7.
- $\ell_B(\mathbf{x}_B) = 0$ m for \mathbf{x}_B on the top and bottom boundaries.

Additionally, the two injection wells ($j = 1, 2$) are equipped with fixed temperature boundary conditions during injection and zero heat transfer thereafter, that is, for $\mathbf{x}_j \in \Gamma_j$:

$$\begin{aligned} T(\mathbf{x}_j) &= T_{\text{well}} \text{ if } Q_j > 0 \\ \nabla T \cdot \mathbf{n} &= 0 \text{ if } Q_j = 0. \end{aligned} \quad (25)$$

Initial Conditions. The CSP 11B is initialized at $t = -3.1536 \times 10^{10}$ seconds (1,000 years before injection begins). The initial condition is given by an initially stagnant water-filled reservoir following the geothermal gradient:

$$s_w = 1, \chi_w^{\text{H}_2\text{O}} = 1, \mathbf{u}_\alpha = 0, \text{ and } T(\mathbf{x}) = T_{\text{geo}}(z). \quad (26)$$

To make the initial condition well-posed, we specify a pressure at the center of Well 1 of 3.0×10^7 Pa. Due to the possibility of natural thermal convection, this initial condition is discussed in more detail in the section “Initial State for Versions 11B and 11C.”

Facies Properties. The geometry contains seven facies, six permeable and one impermeable. These provide the definition of the material properties, as given in **Tables 4 and 5**. The material properties are synthetic and are chosen to be characteristic of storage reservoirs at the Norwegian Continental Shelf.

	Horizontal Intrinsic Permeability, k_h (m ²)	Porosity, ϕ (–)	Immobile Wetting Saturation, $s_{w,imm}$ (–)	Rock Heat Conductivity, κ_s (W m ⁻¹ K ⁻¹)	Diffusion Constants, D_w (m ² s ⁻¹)	Diffusion Constants, D_g (m ² s ⁻¹)
Facies 1	1.0×10 ⁻¹⁶	0.1	0.32	1.90	10 ⁻⁹	2×10 ⁻⁸
Facies 2	1.0×10 ⁻¹³	0.2	0.14	1.25	10 ⁻⁹	2×10 ⁻⁸
Facies 3	2.0×10 ⁻¹³	0.2	0.12	1.25	10 ⁻⁹	2×10 ⁻⁸
Facies 4	5.0×10 ⁻¹³	0.2	0.12	1.25	10 ⁻⁹	2×10 ⁻⁸
Facies 5	1.0×10 ⁻¹²	0.25	0.12	0.92	10 ⁻⁹	2×10 ⁻⁸
Facies 6	2.0×10 ⁻¹²	0.35	0.1	0.26	10 ⁻⁹	2×10 ⁻⁸
Facies 7	0	0	N/A	2.00	0	0

Table 4—Facies properties for 11B and 11C that vary between facies.

Immobile nonwetting saturation, $s_{n,imm}$ (–)	0.1
Max. capillary pressure, $p_{cap,max}^*$ (Pa)	3×10 ⁷
Shape exponent capillary pressure, c_2 (–)	1.5
Dispersivity, E (m)	10
Rock specific heat capacity, C_s (kJ kg ⁻¹ K ⁻¹)	8.5×10 ⁻¹
Rock density, ρ_s (kg m ⁻³)	2500
Shape exponents relative permeability, $c_{\alpha,1}$ (–)	1.5

Table 5—Facies properties for 11B and 11C that are equal in all facies.

From the horizontal permeability, the full facies permeability is defined based on a 10:1 horizontal to vertical anisotropy ratio as

$$\mathbf{k}(\mathbf{x}) = \begin{pmatrix} k_h(\mathbf{x}) & 0 \\ 0 & 0.1 k_h(\mathbf{x}) \end{pmatrix}. \quad (27)$$

We define capillary entry pressure based on the Leverett J -scaling:

$$p_{\text{entry}} = \sqrt{\frac{\phi}{k_x}} \cdot 6.12 \times 10^{-3} \text{ N/m}, \quad (28)$$

where the value $6.12 \times 10^{-3} \text{ N m}^{-1}$ is based on Abdoulghafour et al. (2020).

Operational Conditions. CO₂ injection protocol:

- Both wells are inactive, $Q_1(t) = Q_2(t) = 0$ for $t \leq 0$.
- CO₂ injection in Well 1 at constant rate $Q_1(t) = 0.035 \text{ kg s}^{-1}\text{m}^{-1}$ at $T_{\text{well}} = 10^\circ\text{C}$ for $0 < t \leq 1.5768 \times 10^9$ seconds (continuous injection for 50 years).
- CO₂ injection in Well 2 with rate $Q_2(t) = 0.035 \text{ kg s}^{-1}\text{m}^{-1}$ at $T_{\text{well}} = 10^\circ\text{C}$ for $7.884 \times 10^8 < t \leq 1.5768 \times 10^9$ seconds (start after 25 years and end 25 years later).

Monitor CO₂ flow and transport until the final time $t = 3.1536 \times 10^{10}$ seconds (1,000 years).

Measurables. The same measurables as for CSP 11A (defined in the section “Measurables”) also apply to CSP 11B. In addition, we request CO₂ accumulated in boundary volumes.

CO₂ in Boundary Volumes (CSP 11B and 11C Only). The total mass of CO₂ in all boundary volumes (CO₂ in any form within the region where $L_B^0 \neq 0$ in the sense defined in the section “Initial and Boundary Conditions”) shall be reported in kilograms.

Data Reporting. Data reporting shall follow the same structure for CSP 11A (detailed in the section “Data Reporting”), with the following changes:

- Sparse data: Shall be reported at 3.1536×10^6 -second intervals (10 data points per year) starting at the injection in the file `spe11b_time_series.csv`, on the same form as in the section “Sparse Data,” with the addition of a final column with values of boundary CO₂ (defined in the section “CO₂ in Boundary Volumes (CSP 11B and 11C Only)”).
- Dense data: A spatial map of all field variables (pressure, saturation, phase composition, and temperature) shall be reported for every 5 years from the start of injection. The spatial maps shall be reported on a uniform Cartesian grid of 840 by 120 cells (10 m by 10 m grid cells from the bottom of the domain). For each temporal snapshot indicated by Y years ($Y = 0, 5, 10, \dots$), cell values should be provided in csv format in the file `spe11b_spatial_map_<Y>.y.csv` on the same form as in the section “Dense Data,” with the addition of a final column with temperature values in degrees Celsius.

- The performance data shall be reported with the same change in temporal and spatial resolution as indicated in Points 1 and 2 above.

Technical Description of CSP 11C

The CSP 11C is a 3D geometry set at field scale and conditions typical of the Norwegian Continental Shelf. Version 11C, due to its 3D structure, induces significant computational overhead relative to 11B. While for 11A and 11B it is feasible to consider grids that fully resolve the development of convective mixing, this may be impossible for 11C. Furthermore, the existing challenges associated with correctly capturing the dynamics near the gas-water contact will be exacerbated. On the other hand, the 3D nature of the domain accommodates the injection volume better, and the pressure buildup seen in Version 11B should be lessened.

Relationship to CSP 11B. The CSP 11C is an arched 3D extrusion of CSP 11B, as illustrated in Fig. 6.

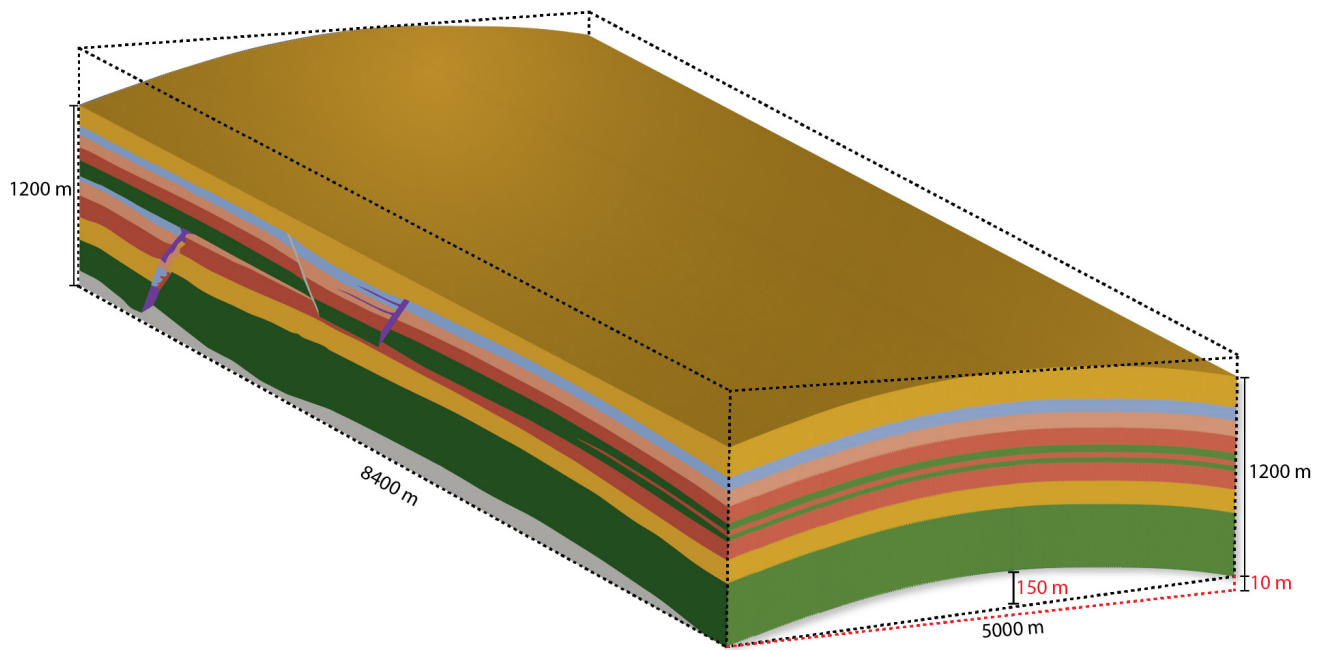


Fig. 6—Sketch of the benchmark geometry for CSP 11C. For a detailed description, please refer to CSP 11C section text and to the caption of Fig. 3.

We summarize the commonalities and differences between CSPs 11B and 11C as follows:

- The governing equations and facies properties for CSP 11B apply to CSP 11C.
- The geometry of CSP 11B is reused in CSP 11C, with the following modification: The depth (along the y -axis) is extended to 5000 m and deformed such that the top surface forms a parabola elevating the central part of the domain by 150 m. See the section “Definition of Geometry, Well Placement, and Reporting Boxes” for precise definition. We emphasize that we keep the coordinate system oriented with the vertical direction pointing “up” and the origin in the “lower-left” corner of the domain, using the convention that the two horizontal axes are enumerated first, that is, with reference to Fig. 5 coordinate triplets are given as (x, y, z) .
- The geometric scaling affects the definition of Boxes A, B, and C, and the well placements, as detailed in the section “Definition of Geometry, Well Placement, and Reporting Boxes.”
- The initial and boundary conditions, together with the injection schedule, are updated to be consistent with the 3D extension; see specification below.

Definition of Geometry, Well Placement and Reporting Boxes. For a precise definition of the geometry, we consider a reference and a physical configuration, with a mapping between them.

Reference Configuration. Let $U = [0, 8400] \times [0, 5000] \times [0, 1200]$ be the extrusion of the geometry from CSP 11B to a depth of 5000 m, as shown in Fig. 7. That is, for any coordinate triplet $(u, v, w) \in U$, the facies properties are defined only by the first horizontal coordinate u and the vertical coordinate w , according to the geometry defined in the section “Relationship to CSP 11A.”

Mapping. For any reference coordinate triplet $\mathbf{u} = (u, v, w) \in U$ in the reference configuration, we identify a position in physical space as

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix} = \Phi(u, v, w) = \begin{pmatrix} u \\ v \\ w + 150 \left(1 - \left(\frac{v - 2500}{2500} \right)^2 \right) + \frac{v}{500} \end{pmatrix}. \quad (29)$$

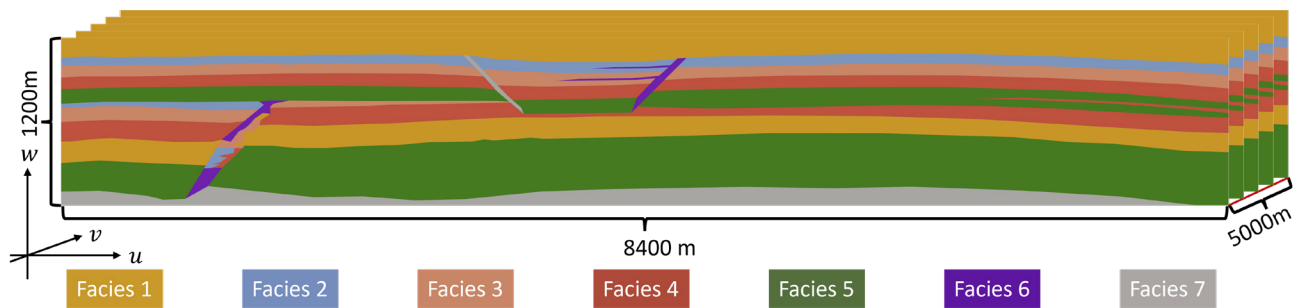


Fig. 7—Sketch of the benchmark geometry for CSP 11C in the reference configuration.

Thus, the domain has a baseline gradient of 2 m/km in the y -direction, so that the back boundary (at $y = v = 5000$) is 10 m higher than the front boundary (at $y = v = 0$). Furthermore, the domain is arched in the y -direction following a parabolic shape with a maximum elevation difference (relative to the baseline gradient) of 150 m at the central ridge of the domain ($y = v = 2500$). The absolute maximum elevation of the ridge is at $y = v = 2541 + 2/3$.

We note that $\Phi(u, v, z)$ is an invertible function for the domain of interest $X = \Phi(U)$, and we denote the inverse as $\Psi = \Phi^{-1}$. For any physical coordinate triplet $\mathbf{x} = (x, y, z) \in X \subset \mathbb{R}^3$, we can thus recover the position in reference configuration as

$$\begin{pmatrix} u \\ v \\ w \end{pmatrix} = \Psi(x, y, z) = \begin{pmatrix} x \\ y \\ z - 150 \left(1 - \left(\frac{y - 2500}{2500} \right)^2 \right) - \frac{y}{500} \end{pmatrix}. \quad (30)$$

The facies distribution, as well as the location of boundaries, for positions $\mathbf{x} \in X$ in the physical configuration can now be obtained based on the facies distribution and boundaries of the reference configuration and the mapping Ψ .

Reporting Boxes. The boxes are adjusted to account for the 3D configuration. We state the (x, y, z) coordinates of the three boxes (measured relative to the lower-left corner of the domain) in terms of the near-bottom-left and far-top-right corners:

Box A: near bottom left (3300, 0, 0), far top right (8300, 5000, 750)

Box B: near bottom left (100, 0, 750), far top right (3300, 5000, 1350)

Box C: near bottom left (3300, 0, 250), far top right (7800, 5000, 550)

Note that the definitions of Boxes A and B extend outside the bottom (resp. top) boundary, and the actual boxes can be truncated to the part within the physical domain X .

Wells and Observation Points. The two injection wells are given as follows. Injection Well 1 is considered as straight (horizontal) in physical space and is open/perforated between the near and far points with (x, y, z) coordinates:

Well 1: near end (2700, 1000, 300), far end (2700, 4000, 300)

Injection Well 2 is considered as curved following the geology in physical space and is thus a straight well in reference space, which is open/perforated between the near and far points with (u, v, w) coordinates:

Well 2: near end (5100, 1000, 700), far end (5100, 4000, 700)

Note in particular that this implies that Well 2 is slightly longer than Well 1, which must be taken into account as the injection rates are given per well length.

The two POPs have (x, y, z) coordinates:

POP 1: (4500, 2500, 655)

POP 2: (5100, 2500, 1255)

Furthermore, to avoid ambiguity, we keep the definition from 11B of the following quantity:

One year is defined as exactly 365 days, containing 31,536,000 seconds.

Initial and Boundary Conditions. We define initial and boundary conditions based on a depth of about 2000 m to the top of the defined geometry.

Boundary Conditions. The left, right, front, and back boundaries are defined to have boundary conditions as defined in the section “Initial and Boundary Conditions” for the left and right boundaries. The top and bottom boundaries are defined to have the same boundary conditions as defined in the section “Initial and Boundary Conditions.”

We point out that because the top and bottom boundaries are nonplanar, the temperature boundary condition given in Eq. 20 implies that the temperature on the top boundary varies between a minimum temperature of about 36.12°C at the top of the arch and a maximum of 40°C where the top boundary meets the front. A similar variation applies to the bottom boundary. The two injection wells ($j = 1, 2$) are equipped with fixed temperature boundary conditions during injection, thereafter zero heat transfer, as stated in Eq. 24.

Initial Conditions. The CSP 11C is initialized at $t = -3.1536 \times 10^{10}$ seconds (1,000 years before injection). The initial condition is given by an initially stagnant water-filled reservoir following the geothermal gradient, as stated in Eq. 25. To make the initial condition well-posed, we specify a pressure at the centerline of Well 1 of 3.0×10^7 Pa.

Facies Properties. The geological model contains seven facies, six permeable and one impermeable. These have properties as given in Tables 4 and 5, and the entry pressure follows the scaling given in Eq. 27.

From the horizontal permeability, the full facies permeability is defined based on a 10:1 horizontal to vertical anisotropy ratio in the reference configuration as

$$\hat{\mathbf{k}}(\mathbf{u}) = \begin{pmatrix} k_h(\mathbf{u}) & 0 & 0 \\ 0 & k_h(\mathbf{u}) & 0 \\ 0 & 0 & 0.1 k_h(\mathbf{u}) \end{pmatrix}. \quad (31)$$

The permeability at a point $\mathbf{x} = \Phi(\mathbf{u})$ in the physical configuration is then given by the standard transformation rules as

$$\mathbf{k}(\mathbf{x}) = \frac{1}{J(\mathbf{u})} \mathbf{F}(\mathbf{u}) \hat{\mathbf{k}}(\mathbf{u}) \mathbf{F}^T(\mathbf{u}), \quad (32)$$

where

$$\mathbf{F}(\mathbf{u}) = \nabla \Phi = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & -\frac{3}{25} \left(\frac{v-2500}{2500} \right) + \frac{1}{500} & 1 \end{pmatrix}, \quad (33)$$

and $J(\mathbf{u}) = \det(\mathbf{F}(\mathbf{u})) = 1$.

This definition of permeability ensures that the anisotropy follows the layering in the y -direction but intersects the layering in the x -direction. This captures, though only conceptually, the computational difficulties associated with both the geological situations of large-scale deformation and erosion surfaces.

Operational Conditions. CO₂ injection protocol:

1. Both wells are inactive, $Q_1(t) = Q_0(t) = 0$ for $t \leq 0$.
2. CO₂ injection in Well 1 with a total rate of 50 kg s⁻¹ at $T_{\text{well}} = 10^\circ\text{C}$ for $0 < t \leq 1.5768 \times 10^9$ seconds (continuous injection for 50 years). Because Well 1 is 3000 m long, this corresponds to $Q_1(t) \approx 1.667 \times 10^{-2}$ kg m⁻¹s⁻¹ (mass per length per time).
3. CO₂ injection in Well 2 with a total rate of 50 kg s⁻¹ at $T_{\text{well}} = 10^\circ\text{C}$ for $7.884 \times 10^8 < t \leq 1.5768 \times 10^9$ seconds (start after 25 years and end 25 years later). Because Well 2 is about 3002.6 m long, this corresponds to $Q_2(t) \approx 1.665 \times 10^{-2}$ kg m⁻¹s⁻¹.

Monitor CO₂ flow and transport until the final time $t = 3.1536 \times 10^{10}$ seconds (1,000 years). The injection rates correspond to about 1.6 Mt/y for each well, thus a total injected mass of about 118 Mt.

Measurables. The same measurables as for CSP 11B (defined in the section “Measurables”) also apply to CSP 11C.

Data Reporting. Data reporting shall follow the same structure for CSP 11B (detailed in the section “Data Reporting”), with the following changes:

4. Sparse data: Shall be reported at 3.1536×10^6 -second intervals (10 data points per year) starting at the injection in a file `spe11c_time_series.csv`.
5. Dense data: A spatial map of all field variables (pressure, saturation, phase composition, and temperature) shall be reported for every 5 years from the start of injection. The spatial maps shall be reported on a uniform Cartesian grid relative to the reference configuration of 168 by 100 by 120 cells (50 m by 50 m by 10 m grid cells from the bottom of the domain). For each temporal snapshot indicated by Y years, $Y = 0, 5, 10, 15, 20, 25, 30, 35, 40, 45, 50, 75, 100, 150, 200, 250, 300, 350, 400, 450, 500, 600, 700, 800, 900, 1,000$ (26 reporting times) cell values should be provided in csv format in the file `spe11c_spatial_map_<Y>.y.csv` on the same form as in the section “Data Reporting,” with the addition of a final column with temperature values in degrees Celsius.
6. The performance data shall be reported with the same change in temporal and spatial resolution as indicated in Points 1 and 2 above.

Remarks

We do not expect that it is possible at the time of issuing this CSP to solve any of the three versions of this CSP in the classical mathematical sense (grid-converged numerical approximation within computable error bounds). Moreover, based on our experience, we expect that even getting the various versions of the CSP to run will require careful choices in terms of how to approximate the spatial variable (i.e., grids), the constitutive functions, and parameters in the computational algorithms. In this section, we highlight some experiences that may be useful to those attempting to simulate the CSP for the first time.

Considerations for Version 11A. Several quantitative observations can be made that guide the numerical approximation choices, as illustrated by the results and discussion presented in the numerical studies of the physical experiment described in the introduction to the section “Technical Description of CSP 11A” [see, e.g., Flemisch et al. (2023); Saló-Salgado et al. (2023); Green et al. (2023); Wapperom et al. (2023)]. Some of these are:

- Grid resolution: A large part of the domain will not see substantial gradients in the variables and can be represented by relatively coarse grids. On the other hand, the gas-water interface (Fig. 8B) is quite sharp and will require a very fine grid to resolve accurately. Similarly, the onset of convective mixing (Fig. 8D) happens at a centimeter scale, suggesting a grid resolution on the order of millimeters to resolve accurately.
- Constitutive functions: The capillary pressure in the coarser sands (Facies 2–5) is relatively small, and gravity segregation dominates even during the injection phase. Thus, the saturation is almost binary (discontinuous). If these discontinuities are not resolved by the grid, it may be advantageous to upscale the constitutive functions to the scale of the grid (likely leading to less nonlinear relative permeabilities).
- Maximum capillary pressure: Gas-phase CO₂ does not enter any of the seal facies (Facies 1). Considering the elevation of the spill point, the gas column thus does not exceed 10–12 cm height. Correspondingly, it is not expected that capillary pressures exceeding 10–12 cm water column (1000–1200 Pa) will appear in the domain. As such, modifying the capillary pressure for values above this value should not change substantially the solution (e.g., we expect that using a value of $p_{\text{cap,max}} = 2500$ Pa will not substantially alter the solution).

- Pressure boundary: Because the CO₂ is in the gas phase, the compressibility is high, and the volume is therefore quite sensitive to pressure variations. As such, care should be taken if approximating the pressure boundary conditions.

Considerations for Versions 11B and 11C. In addition to the considerations presented in the sections “Technical Description of CSP 11B” and “Technical Description of CSP 11C,” some more detailed comments can be made based on theoretical considerations.

- Grid resolution: Gravity-driven convective mixing is also expected to be important for 11B and 11C. Using theoretical estimates (see, e.g., Riaz et al. 2006; Elenius et al. 2012) and parameters from Facies 5, we expect an onset time of a few years with a critical wavelength of less than 5 m. This indicates that a grid-converged solution may require grid cells in the order of a meter or less. On the other hand, suitable scale separation may exist for upscaled models of convection to be applicable for coarser grids.
- Maximum capillary pressure: As for 11A, there is a finite limit on the possible height of a gas column, and therefore it is likely that a significantly lower value of cutoff for the capillary pressure can be used without altering the solution.
- Bottom boundary: The lowest facies is impermeable; however, it does still conduct heat. This leads to two alternatives—either including it as part of the domain or asserting the boundary conditions above the facies. In this latter case, care must be taken to implement thermal boundary conditions that are consistent.

Dispersion. If coarse grids are applied, it is commonly considered that the numerical dispersion will dominate the physical diffusion and dispersion and that the terms related to physical diffusion and dispersion are not necessary to include explicitly. On the other hand, physical diffusion is needed when considering grid convergence studies; otherwise, there is no lowest wavelength for convective mixing, and a grid-converged solution cannot be computed.

The threshold between what is considered “coarse” and “fine” depends on the particular numerical method, but as a rule of thumb, this is proportional to the dispersivity (about 1 cm for 11A and about 10 m for 11B and 11C).

Vertical Equilibrium Pressure and Saturation Distribution. Capillary barriers are important in excluding gas from the seal facies and also for the migration patterns in the upper reservoir, where the facies are fining upwards. To give some intuition to this for those who are unfamiliar with capillary barriers in these systems, we exemplify the typical pressure and saturation under a capillary barrier for a 1D system in equilibrium in Fig. 8. This example is based on the exact solution to the hydrostatic system when density variations are negligible. As can be seen, the saturation is nearly independent of vertical elevation near the discontinuity when the lower material properties correspond to Facies 4 and 5. We note that the sharpness in transition of the saturation depends completely on the shape of the capillary pressure function and must be seen in relation to the vertical extent. Indeed, for finer sands, such as Facies 3, we see more gradual saturation changes.

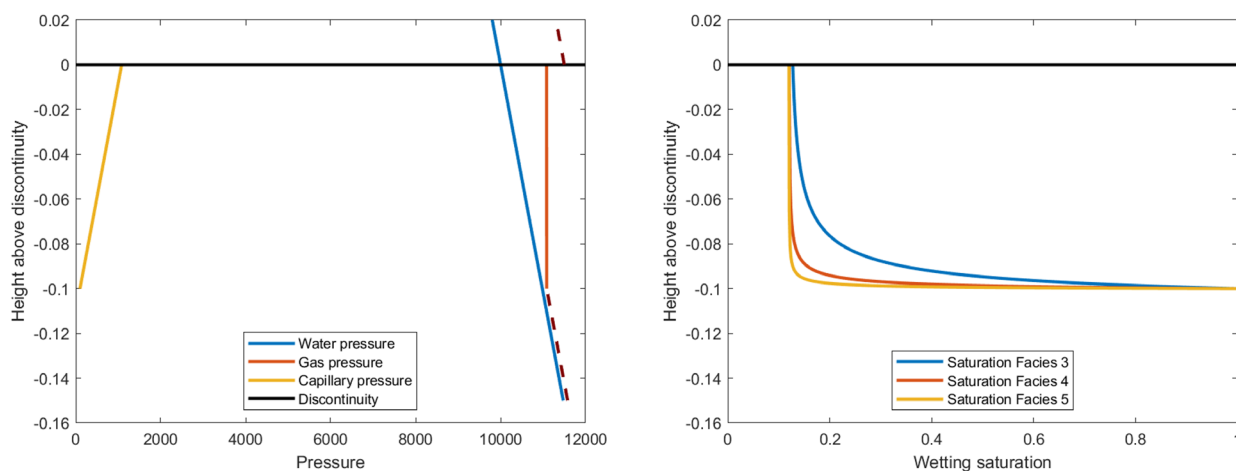


Fig. 8—Pressure and saturation distribution near hypothetical discontinuities between Facies 1 (above discontinuity) and Facies 3–5 (below the discontinuity) for Version 11A, assuming equilibrium pressure and saturation. The left figure shows the phase pressures corresponding to a gas column with a 10-cm height, based on Facies 3 being the lower facies. Dashed lines indicate the “virtual” gas pressures obtained by adding the entry pressure to the water pressure for the two facies. The right figure shows the saturation profile if the lower facies is Facies 3, 4, or 5, respectively. The shape of the curves is exactly the same as if capillary pressure were plotted instead of height, as can be seen by comparison to Fig. 4.

A detail plotted in Fig. 8 (left) is the “virtual” gas pressure in regions with no gas saturation. If an additional amount of gas was introduced in the system, this would shift the gas-water contact downward, until the point where the real gas pressure immediately below the discontinuity (solid red line at negative heights) would equal the “virtual” gas pressure immediately above the discontinuity (dashed red line at positive heights). When pressure continuity is thus achieved, the capillary barrier will no longer be able to sustain the gas column, and gas will begin to migrate into the facies above the discontinuity.

While the above discussion is in the context of 11A, entry pressure effects are also present in 11B and 11C.

Initial State for Versions 11B and 11C. Both Versions 11B and 11C are initialized at 1,000 years before injection, based on a static water column and constant geothermal gradient, as defined in the section “Initial and Boundary Conditions.” In particular, this implies that the vertical pressure at the initial state, $p_{w,0}(z)$, is given by a hydrostatic column satisfying:

$$p_{w,0}(z) = 3 \times 10^7 \text{ Pa} - g \int_{300 \text{ m}}^z \rho_w(p_{w,0}(z'), T_{\text{geo}}(z')) dz' \quad (34)$$

Here, 300 m appears as the vertical elevation of Well 1, and 3×10^7 Pa is the specified pressure at this well.

Fig. 9 shows water and CO₂ densities based on the initial pressure distribution and geothermal gradient. As seen in the figure, the water density is decreasing with depth due to the thermal expansion being of greater importance than the mechanical compression. The profile of water density with depth indicates that water convection cells may appear in the domain.ⁱⁱⁱ By initializing the CSP 1,000 years before injection, we therefore provide some time both for the thermal profile to equilibrate (in response to the facies-dependent thermal conductivity) as well as potential water convection to start. On the other hand, we do not expect that 1,000 years is sufficient to calculate a true equilibrium state (if such exists), and the pre-injection simulation period should therefore be considered a compromise between computational cost and establishing a reasonable initial state.

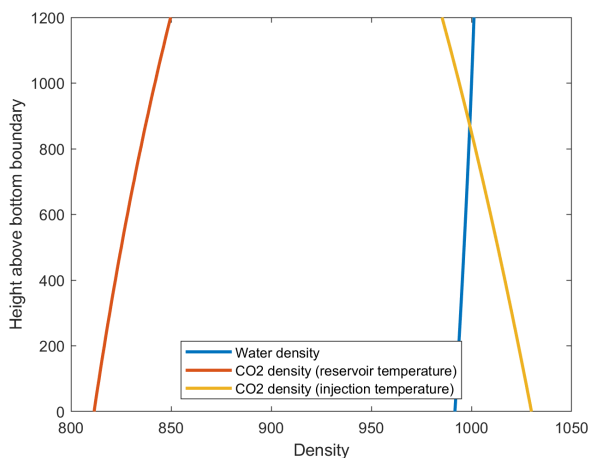


Fig. 9—Density of water and CO₂ for the initial state of CSP 11B. The CO₂ density is plotted both at reservoir temperature (based on the geothermal gradient) and the injection temperature (10°C).

Also evident from Fig. 9 is that the injected CO₂ is denser than the ambient water but is significantly lighter than water at reservoir temperatures. Therefore, some injected CO₂ may sink as the near-well region is cooled by the injection; however, in general CO₂ will rise and accumulate under the low-permeable facies.

We remark that formation water in real reservoirs will in general be saline brines, leading to higher densities than those used in this CSP. The effects described in this section are therefore not necessarily expected to be common. However, prospective storage sites do exist where injection conditions for CO₂ lead to densities close to or above the formation water, and the dynamics are therefore a realistic challenge for reservoir simulation.

Funding

ARK acknowledges funding from the University of Bergen for a sabbatical visit and the Stanford Center for Carbon Storage. BF thanks the German Research Foundation (DFG) for supporting this work by funding SFB 1313, Project Number 327154368.

Acknowledgments

People: In addition to those mentioned in the main text above, the authors thank all of those who have made contributions to this CSP definition through discussions, exchanges of ideas, and critical comments. These include, but are not limited to, Jakub W. Both and Eirik Keilegavlen (U. of Bergen), Denis Voskov (TU Delft), Hamdi Tchelepi (Stanford U.), Ruben Juanes (Massachusetts Institute of Technology), Rainer Helmig (U. of Stuttgart), Sarah E. Gasda (Norwegian Research Center), Alberto Cominelli (Eni SpA), and all participants in the “FluidFlower International Benchmark Study,” who are coauthors of Flemisch et al. (2023): Holger Class, Mojdeh Delshad, Florian Doster, Jonathan Ennis-King, Jacques Franc, Sebastian Geiger, Dennis Gläser, Christopher Green, James Gunning, Hadi Hajibeygi, Samuel J. Jackson, Mohamad Jammoul, Satish Karra, Jiawei Li, Stephan K. Matthäi, Terry Miller, Qi Shao, Catherine Spurin, Philip Stauffer, Hamdi Tchelepi, Xiaoming Tian, Hari Viswanathan, Denis Voskov, Yuhang Wang, Michiel Wapperom, Mary F. Wheeler, Andrew Wilkins, AbdAllah A. Youssef, and Ziliang Zhang.

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ⁱⁱⁱStability analysis indicates that Facies 5 in the lower reservoir is permeable and large enough to be near the critical Rayleigh number for convection to appear.

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